

## Task 1 (20%): System dynamics: From response to model

Consider a process described by the transfer function model

$$y = h_p(s)u. \quad (1)$$

The transfer function  $h_p(s)$  could be a function of the system gain  $K$ , time delay  $\tau$ , system transmission zero  $\tau_z$  and time constants  $T_1$  and/or  $T_2$ .

- a) Given the input and output transient responses,  $u = u(t)$  and  $y = y(t)$  respectively, as illustrated in Figure 1. Propose the structure of the corresponding transfer function  $h_p(s)$  ?
- b) Given the input and output transient responses,  $u = u(t)$  and  $y = y(t)$  respectively, as illustrated in Figure 2. Propose the structure of the corresponding transfer function  $h_p(s)$  ?
- c) Given the input and output transient responses,  $u = u(t)$  and  $y = y(t)$  respectively, as illustrated in Figure 3. Propose the structure of the corresponding transfer function  $h_p(s)$  ?
- d) Given the input and output transient responses,  $u = u(t)$  and  $y = y(t)$  respectively, as illustrated in Figure 4. Propose the structure of the corresponding transfer function  $h_p(s)$  ?

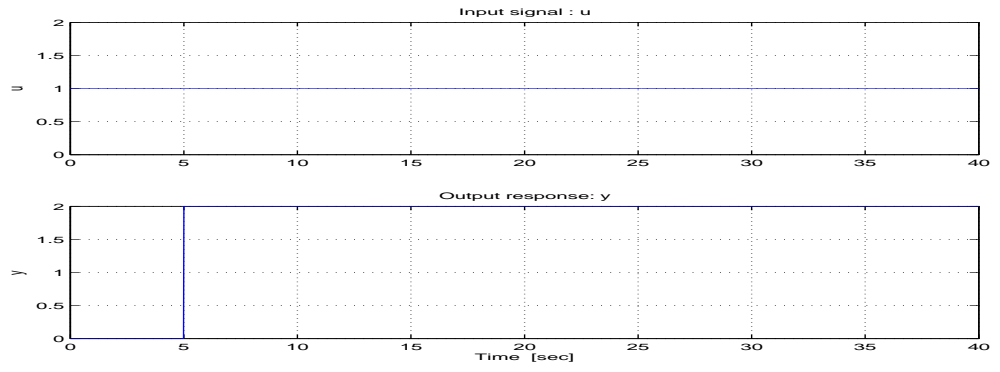


Figure 1: Time response of dynamic system from input  $u$  to output  $y$ .

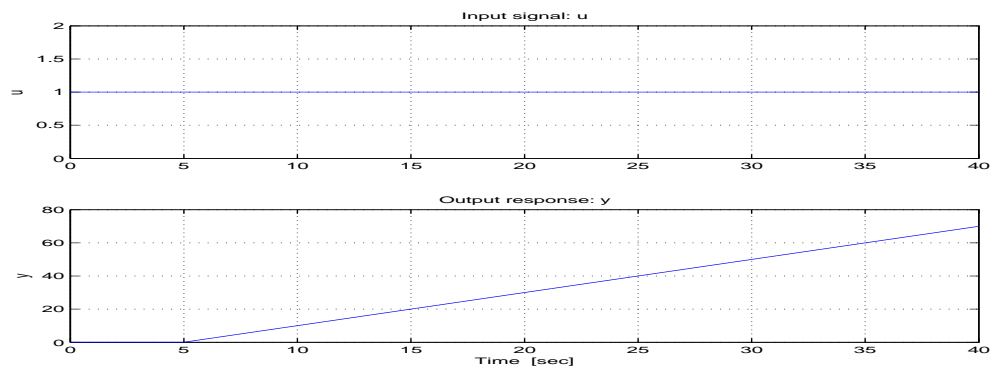


Figure 2: Time response of dynamic system from input  $u$  to output  $y$ .

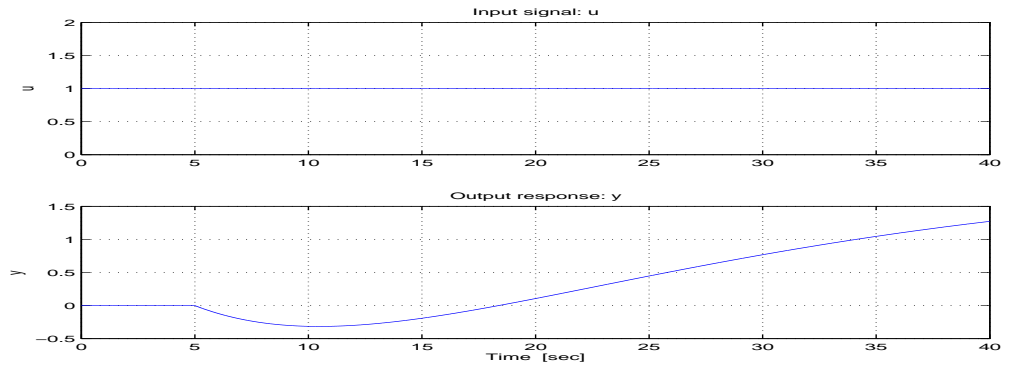


Figure 3: Time response of dynamic system from input  $u$  to output  $y$ .

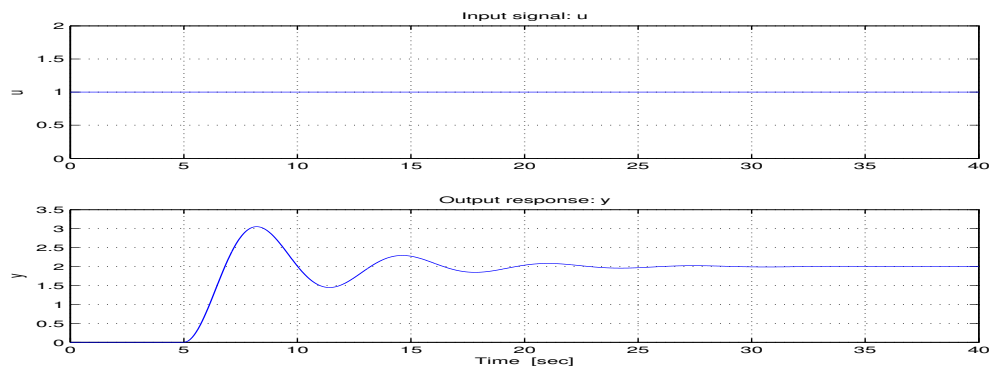


Figure 4: Time response of dynamic system from input  $u$  to output  $y$ .

## Task 2 (20%): PID-control, the SIMC method

Consider a process described by the transfer function model

$$y = h_p(s)u + h_v(s)c. \quad (2)$$

The process is controlled by a controller of the form

$$u = h_c(s)(r - y). \quad (3)$$

The feedback control system is illustrated in Figure (5).

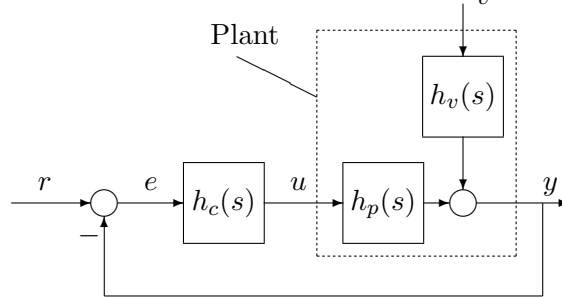


Figure 5: Standard feedback system. Plant described by transfer functions  $h_p(s)$  and  $h_v(s)$ , controller with transfer function  $h_c(s)$ .

a) Give a short description of the SIMC (also known as the Skogestad) method for tuning PID controllers. Comment in particular upon:

- Model requirement.
- As an illustrative example use SIMC tuning on a model  $h_p(s) = K \frac{e^{-\tau s}}{1+Ts}$ .

b) Consider the feedback control system in Figure (5).

- Find the transfer functions  $h_{ry}(s)$  and  $h_{vy}(s)$  from the reference,  $r$ , and the disturbance  $v$  to the output measurement,  $y$ , in the model

$$y = h_{ry}(s)r + h_{vy}(s)v. \quad (4)$$

I.e. find expressions for  $h_{ry}(s)$  and  $h_{vy}(s)$  ?

- Assume  $v = 0$ . Specify a desired transfer function  $h_{ry}(s)$  for the controlled system (closed loop set-point response)? We want  $y \approx r$ .

c)

- Find an expression for the controller transfer function,  $h_c(s)$ , as a function of the time delay transfer function  $e^{-\tau s}$  and the model transfer function  $h_p(s)$  for the process.
- Comment upon the approximation for  $e^{-\tau s}$  used in SIMC ? Find the resulting controller transfer function  $h_c(s)$  ?

d) Given a 4th order process model as follows

$$h_p(s) = K \frac{e^{-s}}{(1 + Ts)^4}. \quad (5)$$

with gain  $K$  and time constant  $T$  with multiplicity  $n = 4$ .

- Use the half rule for model reduction and formulate a 2nd order model approximation of the form

$$h_p(s) = K \frac{e^{-\tau s}}{(1 + T_1 s)(1 + T_2 s)}, \quad (6)$$

for the transfer function in Equation (5). Find the gain  $K$ , the time delay  $\tau$  and the time constants  $T_1$  and  $T_2$  in the model approximation Equation (6) ?

- Find the controller  $h_c(s)$  by the SIMC (Skogestad) method. What type of controller is this?

### Task 3 (25%): PID, SIMC, Frequency analysis

a) Assume that the process,  $h_p(s)$ , is modeled by a 2nd order process of the form

$$h_p(s) = k \frac{e^{-\tau s}}{\tau_0^2 s^2 + 2\tau_0 \xi s + 1}. \quad (7)$$

- What are the definitions for the parameters  $\xi$  and  $\tau_0$  in in the model (7).
- When is the process oscillating ?
- Find the controller  $h_c(s)$  by the SIMC (Skogestad) method.
- What type of controller is this?

b) Given a plant  $y = h_p(s)u$  with model

$$h_p(s) = ke^{-\tau s}. \quad (8)$$

Find a reasonable controller  $h_c(s)$  for this plant described by (8) ?

c) Given a plant  $y = h_p(s)u$  with model as a pure time delay

$$h_p(s) = k \frac{e^{-\tau s}}{s}. \quad (9)$$

Find a P-controller  $h_c(s)$  for this plant described by (9) ?

d) Given a feedback system as illustrated in Figure (5).

Consider a PI controller,  $h_c(s)$ , and an integrating plus time delay process,  $h_p(s)$ , given by

$$h_c(s) = K_p \frac{1 + T_i s}{T_i s}, \quad h_p(s) = k \frac{e^{-\tau s}}{s}, \quad (10)$$

where  $K_p$  and  $T_i$  are the PI controller parameters,  $k$  is the gain velocity (slope of the integrator) and  $\tau$  the time delay.

- Write down an expression for the loop transfer function,  $h_0(s)$ .
- e) Assume for simplicity that we use an approximation  $e^{-\tau s} \approx 1$  for the time delay (same as neglecting the time delay in the model, Eq. (10)).

The set-point response transfer function may then be written as

$$\frac{y}{r} = \frac{\rho(s)}{\pi(s)} \quad (11)$$

where the characteristic polynomial  $\pi(s)$  may be written on standard 2nd order form as follows

$$\pi(s) = \tau_0^2 s^2 + 2\zeta\tau_0 s + 1. \quad (12)$$

Here  $\tau_0$  is the response time and  $\zeta$  the relative damping coefficient.

- Find expressions for the coefficients  $\tau_0^2$  and  $2\zeta\tau_0$  in the characteristic polynomial Eq. (12) as a function of the PI controller parameters  $K_p$ ,  $T_i$  and the gain velocity parameter  $k$ .
- Assume that we prescribe a unit relative damping, i.e.  $\zeta = 1$ . Find expressions for the PI controller parameters  $K_p$  and  $T_i$  as a function of a prescribed response time  $\tau_0 > 0$ . Notice: Use the P-controller from 3c) as  $K_p$  !

## Task 4 (20%): PID controller

Given a PID controller in the Laplace plane

$$h_c(s) = K_p \frac{1 + T_i s}{T_i s} + K_p T_d s = K_p + \frac{K_p}{T_i s} + K_p T_d s, \quad (13)$$

such that the control is generated by

$$u(s) = h_c(s)e(s) \quad (14)$$

where  $e(s) = r - y(s)$  is the control error. We are assuming a constant reference signal,  $r$ , in this task.

- Write down a continuous state space model for the PID controller in Equations (13) and (14).
- Find a discrete time state space model for the PID controller in Step 4a) above.  
Use the explicit Euler method for discretization.
- In this subtask you should use the trapezoid method for discretization.

Find a discrete time PID controller in Step 4b) above on so called velocity (incremental, deviation) form, i.e. in such a way that the control is generated by the formula

$$u_k = u_{k-1} + g_0 e_k + g_1 e_{k-1} + g_2 (y_k - 2y_{k-1} + y_{k-2}). \quad (15)$$

You should also write down the expressions for the parameters  $g_0$ ,  $g_1$  and  $g_2$ .

- d) Do you need a model in order to use a PID controller ? The answer is: Yes or No

### Task 5 (15%): Smith predictor

Assume in this task a system described by the following transfer function model

$$y = h_p(s)u + h_v(s)v. \quad (16)$$

- a) Answer the following:
- When may it make sense to use a Smith predictor?
  - Sketch a block diagram of a system controlled by a Smith predictor.
  - Give a short description of the different elements in the Smith predictor.
- b) Find the transfer function from the reference  $r$  to the system output  $y$  in the Smith predictor.
- c) Find the transfer function from the disturbance  $v$  to the system output  $y$  in the Smith predictor.