

**Final Exam**

**Course SCE1106 Control theory with  
implementation (theory part)**

**Thursday December 17, 2015**

**kl. 9.00-12.00**

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December 14, 2015

## Task 1 (25%): PID-control, the SIMC method

Consider a process described by the transfer function model

$$y = h_p(s)u. \quad (1)$$

The process is to be controlled by a controller of the form

$$u = h_c(s)(r - y). \quad (2)$$

The feedback control system is illustrated in Figure (1).

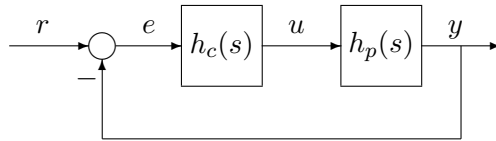


Figure 1: Standard feedback system. Plant described by a transfer function model  $h_p(s)$  and controller with transfer function  $h_c(s)$ .

- Give a short description of the SIMC (also known as the Skogestad) method for tuning PID controllers.
- Consider the feedback control system in Figure (1).

- Find the transfer function  $h_{ry}(s)$  from the reference,  $r$ , to the output measurement,  $y$ , in the transfer function model

$$y = h_{ry}(s)r. \quad (3)$$

I.e. find an expression for  $h_{ry}(s)$  ?

- Specify a desired transfer function  $h_{ry}(s)$  for the controlled system (closed loop set-point response)? This function should be a function of the plant time delay  $\tau$  and a desired time constant  $T_c$  for the controlled system.

c)

- Find an expression for the controller transfer function,  $h_c(s)$ , as a function of the time delay transfer function  $e^{-\tau s}$  and the model transfer function  $h_p(s)$  for the process.
- Use the simple approximation  $e^{-\tau s} \approx 1 - \tau s$  and find the resulting controller transfer function  $h_c(s)$  ?

d) Given a process with a 2nd order model as follows

$$y = h_p(s)u, \quad (4)$$

where

$$h_p(s) = 2 \frac{e^{-s}}{(1 + 8s)(1 + 2s)(1 + s)}. \quad (5)$$

- Use the half rule for model reduction and formulate a 1st order model approximation of the form

$$h_p(s) = k \frac{e^{-\tau s}}{1 + T_1 s}, \quad (6)$$

for the transfer function in Equation (5). Find the gain  $k$ , the time delay  $\tau$  and the time constant  $T_1$  in the model approximation Equation (6) ?

- Find the controller  $h_c(s)$  by the SIMC (Skogestad) method. What type of controller is this?

e) Assume that the process,  $h_p(s)$ , is modeled by a 2nd order process of the form

$$h_p(s) = k \frac{e^{-\tau s}}{\tau_0^2 s^2 + 2\tau_0 \xi s + 1}. \quad (7)$$

- What are the definitions for the parameters  $\xi$  and  $\tau_0$  in in the model (7).
  - When is the process oscillating ?
  - Find the controller  $h_c(s)$  by the SIMC (Skogestad) method.
  - What type of controller is this?
- f) Specify the poles in the system described by Equation (7) for the following two cases:
- $\xi = 1$ .
  - $\xi > 1$ .
- g) Consider a system where the speed of response  $\tau_0 = 0$  ("infinite" fast system) in Equation (7) such that the system can be described by a pure steady state plus time delay process

$$h_p(s) = k e^{-\tau s}. \quad (8)$$

- Find a controller by Skogestad method.
- What type of controller is this ?

## Task 2 (6%): Frequency analysis

Given a feedback system as illustrated in Figure 2.

a) Consider an PI controller,  $h_c(s)$ , and an integrating plus time delay process,  $h_p(s)$ , given by

$$h_c(s) = K_p \frac{1 + T_i s}{T_i s}, \quad h_p(s) = k \frac{e^{-\tau s}}{s}, \quad (9)$$

where  $K_p$  and  $T_i$  are the PI controller parameters,  $k$  is the gain velocity (slope of the integrator) and  $\tau$  the time delay.

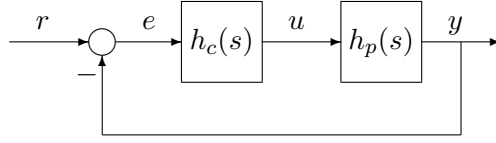


Figure 2: Standard feedback system. Plant described by a transfer function model  $h_p(s)$  and controller transfer function  $h_c(s)$ .

- Write down an expression for the loop transfer function,  $h_0(s)$ .
- b) Assume in this subtask 2b) that we use an approximation  $e^{-\tau s} \approx 1$  for the time delay (same as neglecting the time delay in the model, Eq. (9)).

The set-point response transfer function may then be written as

$$\frac{y}{r} = \frac{h_0}{\pi(s)} \quad (10)$$

where the characteristic polynomial  $\pi(s)$  may be written on standard 2nd order form as follows

$$\pi(s) = \tau_0^2 s^2 + 2\zeta\tau_0 s + 1. \quad (11)$$

Here  $\tau_0$  is the response time and  $\zeta$  the relative damping coefficient.

- Find expressions for the coefficients  $\tau_0^2$  and  $2\zeta\tau_0$  in the characteristic polynomial Eq. (11) as a function of the PI controller parameters  $K_p$ ,  $T_i$  and the gain velocity parameter  $k$ .
- Assume that we prescribe a unit relative damping, i.e.  $\zeta = 1$ . Find expressions for the PI controller parameters  $K_p$  and  $T_i$  as a function of a prescribed response time  $\tau_0 > 0$ .

### Task 3 (12%): Frequency analysis

Given a system which can be described by a first order time delay model

$$h_p(s) = K \frac{e^{-\tau s}}{1 + Ts} \quad (12)$$

where  $T > 0$  is the time constant and  $\tau > 0$  the time delay.

- a) Answer the following: When can we approximate the model Eq. (12) as an integrating plus time delay model ?

$$h_p(s) = k \frac{e^{-\tau s}}{s} \quad (13)$$

Find an expression for the velocity gain (slope of integrator)  $k$  ?

b)

Find an expression for the frequency response of the loop transfer function  $h_0(s)$  found in subtask 3a), on polar form, i.e., such that

$$h_0(j\omega) = |h_0(j\omega)|e^{j\angle h_0(j\omega)}, \quad (14)$$

assuming a P-controller is used.

Find expressions for the magnitude  $|h_0(j\omega)|$  and the phase angle  $\angle h_0(j\omega)$ .

Note: You should in this subtask 3b) use the integrator plus time delay model as in Eq. (13).

c) Answer the following: Use a P controller and the integrating plus time delay model as in Eq. (13)

and find the ultimate gain  $K_{cu}$  and the ultimate period  $P_u = \frac{2\pi}{\omega_{180}}$ .

d) Answer the following: Show how you can estimate the model parameters  $k$  and  $\tau$  in Eq. (13) from the ultimate gain  $K_{cu}$  and the ultimate period  $P_u$ . ?

## Task 4 (9%): PID controller

Given a PID controller in the Laplace plane

$$h_c(s) = K_p \frac{1 + T_i s}{T_i s} + K_p T_d s = K_p + \frac{K_p}{T_i s} + K_p T_d s, \quad (15)$$

such that the control is generated by

$$u(s) = h_c(s)e(s) \quad (16)$$

where  $e(s) = r - y(s)$  is the control error. We are assuming a constant reference signal,  $r$ , in this task.

a) Write down a continuous state space model for the PID controller in Equations (15) and (16).

b) Find a discrete time state space model for the PID controller in Step 4a) above.

Use the explicit Euler method for discretization.

c)

In this subtask you should use the explicit Euler method for discretization.

Find a discrete time PID controller in Step 4a) above on so called velocity (incremental, deviation) form, i.e. in such a way that the control is generated by the formula

$$u_k = u_{k-1} + g_0 e_k + g_1 e_{k-1} + g_2 (y_k - 2y_{k-1} + y_{k-2}). \quad (17)$$

You should also write down the expressions for the parameters  $g_0$ ,  $g_1$  and  $g_2$ .

## Task 5 (8%): The PID controller and the Smith Predictor

Given a system described by the following transfer function model

$$y = h_p(s)u + h_v(s)v \quad (18)$$

- a) Do you need a model in order to use a PID controller? The answer is: Yes or No
- b) Answer the following:
- When may it make sense to use a Smith predictor?
  - Sketch a block diagram of a system controlled by a Smith predictor.
  - Give a short description of the different elements in the Smith predictor.
- c) Find the transfer function from the reference  $r$  to the system output  $y$ .
- d) Find the transfer function from the disturbance  $v$  to the system output  $y$ .